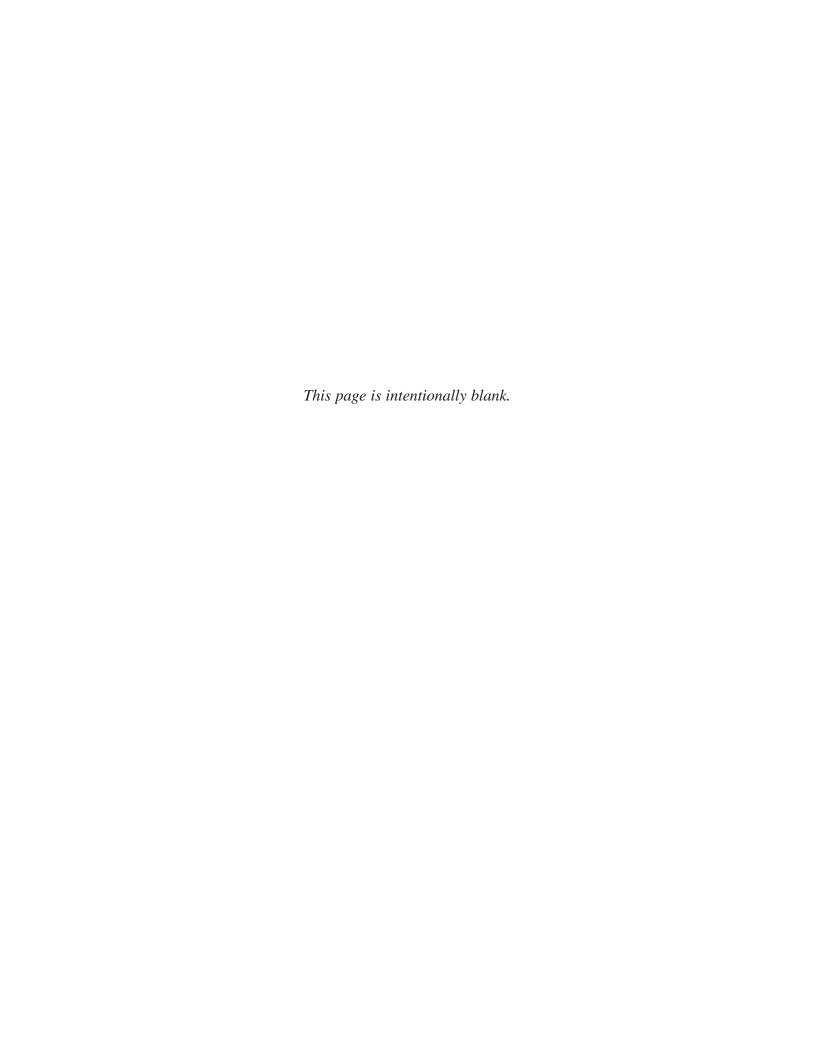
APPENDIX G STUDENT'S T-TEST CALCULATION

he following example details the steps needed to determine the number of samples to be collected, based on historical analytical results and the statistical student's t-test. It has been adapted from information contained in EPA's *An Addendum to the POTW Sludge Sampling and Analysis Guidance Document*, May 1992.



HOW TO DETERMINE THE APPROPRIATE NUMBER OF SAMPLES TO BE COLLECTED

In Chapter 5, the following two equations were provided as a method to determine how many samples should be collected to represent the whole or to determine how many grab samples should be collected to form a composite.

$$S = \sqrt{\frac{\sum \left| \overline{X} - x \right|^2}{N - 1}}$$

Where: S = standard deviation

 \overline{X} = average or mean of all data points

x = individual data points

N = number of data points in the set

 $\sum |\overline{X} - x|^2 = \text{sum of square of the difference between the mean and each individual data point}$

$$N = \frac{T^2 S^2}{\left(RL - \overline{X}\right)^2}$$

Where: N =the minimum samples to characterize sludge

T = value of Student's t for the appropriate number of historical data points at 90% confidence level

S = standard deviation

RL = the regulatory limit for the analyte in question

 \overline{X} = mean of the historical data

To use this method:

- 1) Assemble your historical analytical data for the analyte of interest.
- 2) Calculate the mean or average.
- 3) Calculate the standard deviation using Equation 1.
- 4) Determine the regulatory limit for the analyte chosen.
- 5) Find the Student's T value from Table G-1.
- 6) Using the mean, standard deviation, regulatory limit, and value of Student's T determined above, calculate the appropriate number of samples by using Equation 2.

T value at 90% Confidence Level	Table G-1. VALUES FOR STUDENT'S T AT THE 90% CONFIDENCE LEVEL			
2 2,920 3 2,353 4 2,132 5 2,015 6 1,943 7 1,895 8 1,860 9 1,833 10 1,812 11 1,796 12 1,782 13 1,771 14 1,761 15 1,753 16 1,746 17 1,740 18 1,734 19 1,729 20 1,725 21 1,721 22 1,717 23 1,714 24 1,711 25 1,708 26 1,706 27 1,703 28 1,701 29 1,699 30 1,697 40 1,684 50 1,676 60 1,671 70 1,664 90 1,662	Degrees of Freedom (df)	T value at 90% Confidence Level		
2 2,920 3 2,353 4 2,132 5 2,015 6 1,943 7 1,895 8 1,860 9 1,833 10 1,812 11 1,796 12 1,782 13 1,771 14 1,761 15 1,753 16 1,746 17 1,740 18 1,734 19 1,729 20 1,725 21 1,721 22 1,717 23 1,714 24 1,711 25 1,708 26 1,706 27 1,703 28 1,701 29 1,699 30 1,697 40 1,684 50 1,676 60 1,671 70 1,664 90 1,662	1	6.314		
4 2.132 5 2.015 6 1.943 7 1.895 8 1.860 9 1.833 10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.664 90 1.662				
4 2.132 5 2.015 6 1.943 7 1.895 8 1.860 9 1.833 10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.664 90 1.662				
5 2.015 6 1.943 7 1.895 8 1.860 9 1.833 10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662				
6 1.943 7 1.895 8 1.860 9 1.833 10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662				
7 1.895 8 1.860 9 1.833 10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662				
9 1.833 10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.708 28 1.701 29 1.699 30 1.697 40 1.684 50 1.667 80 1.664 90 1.664				
10 1.812 11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	8	1.860		
11 1.796 12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	9	1.833		
12 1.782 13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	10	1.812		
13 1.771 14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	11	1.796		
14 1.761 15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	12			
15 1.753 16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	13	1.771		
16 1.746 17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	14	1.761		
17 1.740 18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	15	1.753		
18 1.734 19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	16			
19 1.729 20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	17	1.740		
20 1.725 21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	18			
21 1.721 22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	19			
22 1.717 23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	20			
23 1.714 24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	21	1.721		
24 1.711 25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	22			
25 1.708 26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	23			
26 1.706 27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	24			
27 1.703 28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	25			
28 1.701 29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	26			
29 1.699 30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	27			
30 1.697 40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	28			
40 1.684 50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	29	1.699		
50 1.676 60 1.671 70 1.667 80 1.664 90 1.662	30			
60 1.671 70 1.667 80 1.664 90 1.662	40			
70 1.667 80 1.664 90 1.662	50			
80 1.664 90 1.662	60	1.671		
90 1.662	70	1.667		
	80	1.664		
100	90	1.662		
100 1.660	100	1.660		
120 1.658	120	1.658		
infinity 1.645	infinity	1.645		

Sample Calculation

Below is a step-by-step example calculation. The objective is to determine the number of composite samples that should be collected during the year to produce statistically valid sludge copper (Cu) concentrations. The following historical Cu data (see Table G-2) will be used.

Table G-2. HISTC	HISTORICAL COPPER DATA		
Date of Sample	Copper Concentration (mg/kg)		
7/24/02	480		
1/13/03	360		
6/11/03	330		
5/15/03	135		
11/6/03	400		
1/7/04	189		
4/12/04	140		
5/27/04	200		
10/26/04	79		
1/27/05	140		
3/22/05	100		
5/27/05	268		

Step 1: Calculate the average Cu concentration, add all the concentrations and divide by the number of values:

Date of Sample	Copper Concentration (mg/kg)	
7/24/02	480	
1/13/03	360	
6/11/03	330	
5/15/03	135	
11/6/03	400	
1/7/04	189	
4/12/04	140	
5/27/04	200	
10/26/04	79	
1/27/05	140	
3/22/05	100	
5/27/05	268	
TOTAL	2821	

Average Copper = $2821 \div 12 = 235$ (rounded to the nearest whole number)

$$\overline{X}$$
 = 235

Appendix G: Student's T-Test Calculation

Step 2: Calculate the standard deviation. Fortunately most spreadsheet applications will perform the calculation for you. To perform the process by hand, subtract each individual Cu concentration from the average concentration. Next, square the difference between the average and individual values and sum the squares. See Table G-3 for an example of these calculations. This sum of squared differences can be inserted into the numerator of Equation 1 above.

Table G-3. CALCULATING THE SUM OF SQUARED DIFFERENCES					
Date of Sample	Cu Concentration (mg/kg)	$\overline{(X}-x)$	$(\overline{X}-x)^2$		
7/24/02	480	-245.00	230400		
1/13/03	360	-125.00	129600		
6/11/03	330	-95.00	108900		
5/15/03	135	100.00	18225		
11/6/03	400	-165.00	160000		
1/7/04	189	46.00	35721		
4/12/04	140	95.00	19600		
5/27/04	200	35.00	40000		
10/26/04	79	156.00	6241		
1/27/05	140	95.00	19600		
3/22/05	100	135.00	10000		
5/27/05	268	-33.00	71824		
SUM	2821		186941		

The remaining calculation is as follows:

Standard Deviation =
$$\sqrt{\frac{186941}{12-1}}$$
 = 130 (rounded to the nearest whole number)

Step 3: Based on federal regulations, the ceiling limit for Cu is 4300 mg/kg and the pollutant concentration limit is 1500 mg/kg. In this example, we will assume that the facility wants to show compliance with the lower limit.

Going back to Equation 2, we can see that the average, standard deviation, and regulatory limit have been determined. To use the equation, the final value that must be obtained is Student's T at a 90% confidence level. To find Student's T, use Table G-1. First, find the degrees of freedom by subtracting 1 from the number of historical data points you used to determine the average and standard deviation.

Degrees of Freedom (df) =
$$12 - 1 = 11$$

Using Table G-1, locate the Student's T for 11 degrees of freedom (1.796).

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Now all the values can be inserted into Equation 2 to obtain the number of grab samples to form a composite.

Number of composite samples =
$$\frac{1.796^2 \times 130^2}{(1500 - 235)^2} = 0.03$$

This calculation indicates that, based on historical data and the current regulatory limit, one composite sample should be sufficient to ensure that regulatory limits are being met. However, facilities must perform the sampling required by state and federal regulations regardless of the results of this calculation. Also, facility operators should be aware that the results of this calculation are heavily influenced by the variability of the historical data and the regulatory limit. For example, if the regulatory limit were 400 mg/kg, the results would indicate that two samples were needed. As a rule of thumb, if the mean of historical data plus the standard deviation is greater than the regulatory limit, then Equation 2 may be helpful in determining the appropriate sampling frequency or number of samples.

